

Preliminary Geotechnical Interpretive Report for

Silo Ridge Golf Resort Community

Town of Amenia Dutchess County New York

September 14, 2006



Prepared for:

Mr. Stephen Garofalo Higher Ground Country Club Management Company L.L.C. P.O. Box 86, Route 22 Amenia, New York 12501 Preliminary Geotechnical Interpretive Report for

Silo Ridge Golf Resort Community

Town of Amenia Dutchess County New York

September 14, 2006



Project Number: 30631.00

Prepared by:

Capital District Office The Chazen Companies 547 River Street Troy, New York 12180 (518) 273-0055

Orange County (845) 567-1133

Dutchess County (845) 454-3980

North Country (518) 812-0513

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1.0 EXECUTIVE SUMMARY

The Chazen Companies (TCC) conducted a preliminary subsurface investigation to provide geotechnical recommendations for design of a hotel consisting of three separate multi-story buildings, each with potential underground parking in the Town of Amenia, Dutchess County, New York, hereinafter referred to as the "site".

Overburden at the site consists of Silty Sand and Poorly Graded Sand with Silt and Gravel. Bedrock was encountered between El. 582 and El. 542 feet above mean sea level. Groundwater was not observed within the limits of the explorations.

Shallow foundations consisting of reinforced concrete continuous strip footings and isolated spread footings with a soil supported slab are recommended to support the proposed buildings. An allowable bearing capacity of 6 tons per square foot (tsf) is recommended for shallow spread footings for the Northeast and Southeast structures and 3 (tsf) for a soil supported slab. Depending on the design concept chosen for the Southwest structure, we anticipate that an allowable bearing capacity between 2 tsf and 6 tsf is achievable for shallow spread footings and between 1 tsf and 3 tsf for a soil supported slab. However, additional studies are required to develop the entire site, particular the Southwest structure.

Differential settlement could result if a foundation spans over different soil types. Therefore, foundations should be designed to accommodate differential settlement or utilize the lowest allowable bearing capacity to support foundation design. Based on the existing site conditions, the seismic design category for the site is "B" assuming that less than 10 feet of soil will be present between bedrock and building foundations. Overburden soils may be suitable for reuse as common fill for general earthwork and landscaping purposes, but are not recommended for use as fill beneath buildings, pavements or against foundations walls.

Provided the geotechnical recommendations and construction considerations are incorporated in the design and during construction activities, the site is considered suitable for the proposed development.

2.0 INTRODUCTION

Higher Ground Country Club Management Company LLC retained The Chazen Companies (TCC) to provide preliminary geotechnical engineering services described in the Proposal for Professional Services dated July 12, 2006. The authorized scope included planning, coordinating and conducting a preliminary subsurface investigation and preparation of this geotechnical interpretive report.

This report includes interpretation of subsurface conditions, preliminary geotechnical recommendations and feasible foundation alternatives for design of the proposed hotel consisting of three separate multi-story buildings, which may include below grade parking. The site is located within the Town of Amenia, Dutchess County, New York as shown on the Site Location Map included as Figure 1.

3.0 PHYSICAL SETTING

The proposed site for the hotel is west of NYS Route 22 and southeast of the current clubhouse. The proposed site is situated partially on an existing parking area and is adjacent to the main road leading to the existing club house. The site is open and undeveloped with large rock outcroppings observed across the site.

Existing topography indicates that a ridge runs south to north across the middle of the site. The high point on the ridge is located on the southern portion of the proposed site, at El. 590 ft msl. Ground surface elevations decrease gently to the north and west to El. 570 ft msl and to the east to El. 550 ft msl, respectively. Existing site conditions are depicted in Figure 2, Exploration Location Plan.

Elevations noted herein are based on a site survey performed by others utilizing the National Geodetic Vertical Datum of 1929 (NGVD 29).

4.0 SUBSURFACE INVESTIGATION

This section summarizes the results of the subsurface investigation performed at the site in July 2006 in the area of the proposed development.

4.1 Test Boring Explorations

A preliminary subsurface investigation was conducted to characterize the in situ conditions and to recover representative soil and rock samples. Samples were used for both visual classification and laboratory testing to determine the engineering properties at the site. Three test boring explorations, designated SRB-1 through SRB-3, and eight auger probes, designated SRP-1 through SRP-8, were performed within the limits of the site. These explorations were performed to obtain subsurface information at specific points based on the locations of the three proposed buildings.

Proposed exploration locations were marked in the field prior to the subsurface investigation by a TCC representative for utility clearance. In some instances, exploration locations were relocated from marked location due to site conditions. Offset measurements were collected by TCC personnel from the original location to

the as-drilled location to document the actual location of each exploration as shown on Figure 2, Exploration Location Plan.

Test boring explorations were performed on August 7, 2006 and August 8, 2006 by SJB Services, Inc. of Balston Spa, New York. Test boring explorations were advanced to a maximum depth of 29 feet below existing site grades. Explorations were advanced using a CME 550 X all terrain vehicle (ATV) drill rig capable of spinning 3 ¼ inch I.D. hollow stem augers. Soil samples were collected in test boring explorations at approximately 5 foot intervals unless indicated otherwise on the exploration logs. Rock samples were collected in the three test boring explorations using a 5-foot long NX size core barrel with an I.D. of 2 inches.

Explorations were monitored by a TCC representative to advise the driller as to location and depth of borings, to record subsurface activities, and to modify the subsurface investigation as necessary. During soil sample collection, a 2-inch split spoon sampler was driven approximately 2 feet and the number of blows required to drive the sampler every 6 inches were recorded in accordance with ASTM D 1586 to determine the in situ compactness and consistency. The number of blows required to drive the sampler 12 inches, between the 6 and 18 inch interval, is a Standard Penetration Test (SPT) and the total number of blows recorded in this range is the N-value. Split spoon refusal is defined as 50 blows or more recorded within one 6 inch interval. Soil samples collected during the subsurface investigation were visually classified in the field in accordance with the Unified Soil Classification System (USCS) and ASTM D 2488. Logs detailing the explorations were prepared by TCC to document subsurface conditions at the site and are included in Appendix A.

4.2 Subsurface Stratigraphy

Explorations indicate that at least three distinct strata are present within the depth of explorations at the site. However, all strata may not be present at all exploration locations. The stratification lines designating the interface between soil types on the exploration logs represent approximate boundaries. The sequence of strata, starting from existing site grades and working downward, is: Silty Sand, Poorly Graded Sand with Silt and Gravel, and Gneiss. Each stratum is further defined in the following paragraphs.

Silty Sand: A stratum of Silty Sand (SM) was encountered, across a majority of the site, from existing ground surface to a depth up 10 feet, El. 585 to El. 570 ft msl, approximately. This stratum consists of dry, brown, loose sand with some silt, a little to trace of clay and a trace of gravel.

Poorly Graded Sand with Silt and Gravel: A stratum of Poorly Graded Sand with Silt and Gravel (SP-SM) was encountered at existing ground surface to depths between 1.5 ft and 6 ft, El. 567 ft to El. 542 ft msl, approximately, in SRB-1, SRB-2, SRP-2 and SRP-3. However, in the other explorations this stratum underlies the Silty Sand at depths between 1.5 ft to 10 ft, El. 585 ft to El. 570 ft msl, approximately. This stratum consists of dry, gray, very dense sand with some gravel and a little silt.

Bedrock (Gneiss): All explorations terminated on or within Bedrock (Gneiss), which underlies the overburden within the project area as confirmed by three recovered core samples. In addition, exposed bedrock outcrops were observed along the southeastern portion of the ridge.

The depth to bedrock varied across the site from 1.5 feet to 19 feet, El. 582 ft to El. 542 ft msl, approximately. Based on visual observations and measurements of the recovered rock samples during our subsurface investigation the cored rock is a medium hard to hard, gray and white, coarse to fine grained Gneiss, that is moderately to slightly weathered, with horizontal bedding plans and with slight staining and joints that are irregular and smooth. Laboratory results indicated that the unconfined compressive strength for a sample from exploration SRB-2, RC-1 was 4,740 pounds per square inch (psi), which is less than the typical range for this rock, 7,250 psi – 29,000 psi.

A few cobbles were encountered during the investigation, but no boulders. However, greater quantities of cobbles and or boulders could potentially be present within soils encountered at the site.

4.3 Groundwater Condition

Groundwater was not observed during the site exploration based upon field observations and visual classifications of soil samples. Groundwater levels will fluctuate with season, precipitation, nearby construction activity, and other factors.

4.4 Laboratory Analysis

Representative soil and rock samples were selected for geotechnical laboratory testing. The samples were delivered to Atlantic Testing Laboratories in Clifton Park, New York for basic classification testing to verify classifications and rock strength. Field classifications were revised, if necessary, based on the laboratory test results. The following laboratory tests were conducted:

- 2 Natural Moisture Content test,
- 2 Particle-Size Analysis (Mechanical), and
- 1 Unconfined Rock Compression test

Laboratory test results are provided in Appendix B.

5.0 RECOMMENDATIONS

This section presents our geotechnical foundation recommendations for preliminary design of the proposed building based on the subsurface exploration. Our recommendations are in accordance with the Building Code of New York State (BCNYS).

5.1 Preliminary Building Foundation Alternatives

The exact location, elevation or configuration of the proposed structures had not been established at the time of the investigation. However, based on provided footprint dimensions and the subsurface conditions observed during the investigation, the use of shallow foundations, consisting of continuous strip footings and isolated spread footings, if necessary, are suitable foundation alternatives to support the proposed structure in the general location investigated.

5.1.1 Northeast & Southeast Structures

Shallow bedrock, generally, was encountered between 1 and 6 feet in the northeast and southeast portions of the hotel development area. Therefore, the Northeast and Southwest structures, as shown on Figure 3, Conceptual Layout Location Plan, are likely to bear on weathered gneiss bedrock, which can typically provide an allowable bearing capacity between 8 and 12 tons per square foot (tsf). Based on the low Rock Quality Designation (RQD) observed, we recommend an allowable bearing capacity of 6 tsf.

Below grade parking for these two structures is possible, but will require significant rock excavation. The maximum Rock Quality Designation (RQD) observed during the investigation was 26.7%, which indicates the rock is fractured and weathered into a less massive formation that could potentially be excavated without blasting. Additional studies are recommended to further characterize the bedrock within the footprints of these two structures in order to assess excavation requirements.

Care should be taken not to disturb soils at the bearing surface. The zone of influence is defined as a line drawn outward and downward from the lower edge of the footing at a 1 Horizontal: 1 Vertical (1H: 1V) slope as shown on Figure 4, Foundation Detail. Exposed subgrades should be lightly compacted (proofrolled) prior to placement of foundation elements using appropriate construction equipment in large, accessible excavations and hand-guided compaction equipment in smaller excavations where access is limited. All unsuitable soils and disturbed soils should be excavated and replaced with placed and compacted structural fill.

We recommend that installed continuous strip footing foundations and isolated spread footing foundations have minimum lateral dimensions of at least 2 feet and 3 feet, respectively. For isolated spread footings with a lateral dimension less than 3 feet, the allowable soil bearing pressure should be reduced to a value equal to one third of the maximum allowable bearing pressure, multiplied by the least lateral footing dimension (in feet). Foundation elements must be constructed in accordance with the BCNYS, Section 1805.

Total settlement for statically loaded footings designed using the recommended allowable bearing capacity is expected to be less than 1.0 inch and differential settlement (non-uniform settlement) is anticipated to be less than 0.5 inches.

While preparing the slab subgrade, all unsuitable materials, should be overexcavated 12 inches and replaced with compacted structural fill before placing at least 4-inches of stone fill for the slab to bear on, as required by the BCNYS, Section 1807.4.1. A vapor barrier placed between the moisture sensitive slab and placed on compacted stone fill is recommended as per Section 1807.2.1 of the BCNYS.

Design and construction of the slab should take into account potential differential shrinkage between the top and bottom surfaces of the slab that could result in curling. A coefficient of friction of 0.20 should be used between the slab and vapor barrier and 0.35 for concrete cast directly against proofrolled in situ soils or compacted structural fill.

5.2 Site Seismic Characterizations

The on-site soils have been characterized for seismic conditions in accordance with Section 1615 of the BCNYS. Soils at the site are judged not susceptible to liquefaction due to the absence of water based on the exploration, relative density, soil type, and published peak ground acceleration.

A soil supported slab, designed for an allowable bearing capacity of 3 tsf is recommended for each building when founded on placed and compacted stone fill founded on weathered bedrock.

5.1.2 Southwest Structure

The subsurface conditions in the southwest portion of the development site change dramatically from east to west. The subsurface investigation indicates that shallow bedrock is present near the eastern end of the Southwest structure, but the rock drops to a depth of approximately 19 feet in the western end of the structure. Therefore, the concept needs to be further developed before a recommendation can be provided that addresses differential settlement potential, which must be limited to within the tolerable range. The foundation elevation will be a major factor in determining the bearing material and the appropriate allowable bearing capacity to design for. Depending on the foundation elevation and design approach, we anticipate that an allowable bearing capacity for the shallow foundations and a soil supported slab will range between 2 tsf to 6 tsf and 1 tsf to 3 tsf, respectively.

Since structures founded on different soil types have the potential for differential settlement and associated structural symptoms, design of the foundation for the Southwest structure must take the varying bearing materials into account to limit differential settlement. This can be performed in a number of ways including providing a 12 inch layer of compacted, granular fill above bedrock beneath the whole structure, designing foundations to the lowest strength in situ bearing material or designing foundations based on the capacity of a high strength fill material that may approach the strength of the bedrock.

Below grade parking is also possible for this structure, but will require some rock excavation and filling due to the rapid drop in bedrock at the western end of the building. Excavated rock could potentially be used for filling to provide a more uniform bearing surface.

5.1.3 General Foundation Recommendations

The bottom of spread footing foundations, not bearing on bedrock, should be located a minimum of 4 feet below the lowest adjacent ground surface exposed to freezing and the subgrade must be protected from freezing during construction. Spread footings not exposed to freezing temperatures during construction and located beneath continuously heated interior spaces should bear at least 18 inches below the top of the soil supported slab.

Based on the existing site conditions, proposed locations and assuming structure classifications as defined in Table 1604.5 of the BCNYS, we recommend the following:

Category	Main Structures
Seismic Use Group	II
Seismic Importance Factor, I _E	1.25
Site Class	B1
Seismic Design Category	В

^{1.} A Site Class of B was selected assuming that less than 10 feet of soil will be present between the bedrock and the building foundation. If this condition is not achieved, a Site Class of C is more appropriate.

5.3 Foundation Walls

If below grade foundation walls will be utilized at this site, we recommend using the following equivalent fluid pressure values in pounds per cubic foot (pcf) to model lateral earth pressures assuming a level back slope and that no hydrostatic pressures (drained conditions) will be present, an internal friction angle for backfill soil of 34°, and a unit weight of 120 pcf:

Lateral Earth Pressure Type	Equivalent Fluid Unit Weight
At Rest - Static, (Restrained condition at top of wall)	54 pcf
Active (Wall allows for deflection at top)	34 pcf
Passive	350 pcf
Active with Seismic (PGA, 2% PE in 50 years)	46 pcf

Passive pressure resistance is often not incorporated into design to provide an additional factor of safety and for other reasons including the large amount of movement required to mobilize passive resistance and the potential future removal of soil.

Equivalent fluid pressures stated herein do not include safety factors. When recommended equivalent fluid pressures are utilized, appropriate factors of safety for sliding, overturning, and bearing capacity should be applied in the design.

We recommend installation of drainage fill or drainage board against retaining walls to relieve hydrostatic pressures where they could develop by allowing downward flow of water to a perimeter foundation drainage system in accordance with the BCNYS, Sections 1807.4 and 1807.1.3. The drainage system should maintain groundwater at an elevation not less than 6 inches below the bottom of the lowest floor. The system should include a 4 inch diameter (min.) perforated drain pipe encased in stone fill and located adjacent to the spread footing. Installation of a cleanout is also recommended to facilitate maintenance of the drainage system. In addition, we recommend application of damp-proofing materials to the exterior surface of below grade foundation walls, in accordance with the BCNYS, section 1807.2.2.

5.4 Utilities

Utility trenches and established trench invert elevations should be located outside the "zone of influence" of foundation elements. Trench excavation widths should extend a minimum of 12 inches beyond the outer edges of the utility elements to be installed. Exposed subgrades should be lightly compacted (proofrolled) and filled with placed and compacted bedding fill extending 6 inches (minimum) below and above each utility. When utilities are located in trenches below building slabs and pavements, trenches should be backfilled above this point with compacted structural fill up to the proposed subgrade located beneath the building slab or pavement section. In landscaped areas, utility trenches above this point may be backfilled with common fill.

Visible markers at the surface and an underground trace line should be installed along the utility line to facilitate location of the utility in the future.

5.5 Fill Materials

Fill materials shall be free of unsuitable material such as organics, construction debris, cobbles/boulders, frozen material, etc. Stockpiles of fill materials should be maintained to prevent material from fluctuating from the optimum moisture content, freezing, separating due to migration of fine grained soils, and collection of snow or ice within the stockpiles. Fill areas should be cleared of all vegetation, roots, and other organic materials prior to placement of fill. Stockpiled soils may require installation of run-off protection between drainage channels and the stockpile.

Compaction should consist of at least 4 systematic passes using a vibratory roller. In confined areas, hand guided vibratory equipment shall be utilized to compact the soil to the specified criteria. If soil weaving or other disturbance is noticed during compaction, vibratory compaction should be discontinued. Heavy

compaction equipment should not be utilized within 3 feet of foundation and retaining walls. Compaction shall meet the requirements stated below or as approved by a qualified engineer.

5.5.1 Stone Fill & Granular Fill

Stone fill, such as a uniformly graded ¾ inch crushed stone, is recommended for prepared subgrades for slab construction and also for use around perforated drain pipes when used with an appropriate geotextile filter fabric.

Stone fill should be placed in loose lifts not to exceed 8 inches in thickness for heavy compaction equipment and 6 inches for lighter compaction equipment. Prior to placement of stone fill, we recommend placement of a non-woven, geotextile, filter fabric on the prepared subgrade to prevent migration of fines into the stone void space. A fabric should be selected based on the gradation of the surrounding soils.

Granular fill used for drainage along foundation walls should be clean, uniformly graded granular fill, which meets the following suggested gradation:

Sieve Size	Percent Passing by Weight
$\frac{1}{4}$ inch	100
No. 4	50-75
No. 40	10-20
No. 200	0-5

Granular fill should be placed in lifts not exceeding 8 inches loose measure and compacted to 90% of the maximum dry density as defined by ASTM D 1557. Stone fill should not be used against damp-proofed foundation walls unless a protective barrier is used to prevent direct contact between the stone and the damp-proofing.

5.5.2 Structural Fill

Clean, granular, structural fill meeting the following suggested gradation should be placed in lifts not exceeding 8 inches loose measure and compacted to 95% of maximum dry density as defined by ASTM D 1557. Structural fill materials should be adjusted to within +2% and -1% of optimum moisture content to facilitate proper compaction. Structural fill is recommended for backfill within the footprint of the building and above utilities within the "zone of influence".

Sieve Size	Percent Passing by Weight		
3 inch	100		
½ inch	50-85		
No. 4	30-75		
No. 40	10-25		
No. 200	0-8		

5.5.3 Bedding Fill

Bedding fill should be provided and compacted as recommended by the pipe manufacturer for backfill around utilities. If the manufacturer does not provide recommendations for pipe bedding material, a clean, granular, bedding fill meeting the following suggested gradation should be placed in lifts not exceeding 8 inches loose measure and compacted to 92% of maximum dry density as defined by ASTM D 1557.

Sieve Size	Percent Passing by Weight
¼ inch	100
No. 4	70-85
No. 40	10-40
No. 200	0-10

5.5.4 Common Fill

Common fill should consist of inorganic, sand based, granular soils that meet the following basic, gradation requirements:

Sieve Size	Percent Passing by Weight
3 inch	100
No. 40	20-80
No. 200	0-20

Common fill used for site grading and landscaping should be placed in lifts not exceeding 9 inches loose measure and compacted to 90% of the maximum dry density as determined by ASTM D 1557. All fill should be placed to promote positive drainage away from structures.

5.5.5 On-Site Soils

On-site soils are not suitable for use as structural fill as described above due to the high percentage of fine grained soil. Silty Sand may be suitable for use as landscaping fill. Poorly Graded Sand with Silt and Gravel could possibly be used as common fill or bedding fill if screened to remove the larger particles.

6.0 OTHER CONSIDERATIONS

This section presents additional considerations to address excavation and groundwater conditions.

6.1 Excavation

We anticipate that excavation of the on-site soils can be accomplished using conventional earthwork equipment and techniques (i.e., backhoes, scrapers, excavators, or dozers) based on the physical characteristics and relative density of the materials.

Excavation of bedrock is anticipated in order to achieve desired bearing elevations. Typically, the quality of rock increases with depth. Based on the amount of rock recovered during coring from 47% to 100% and calculated RQD's, % to 27%, rock at the site could potentially require alternative methods of excavation such as jack hammering, hoe ramming and blasting. Care should also be taken when excavating due to the presence of existing utilities on the site.

Generally, all temporary cut slope excavations should not be left open or unbraced for extended periods of time. Temporary cuts should be sloped as required for stability in accordance with OSHA regulations and protected from erosion. Based on the subsurface explorations, the on-site soils should, generally, be classified as Type "C" material according to OSHA regulations, but be verified for each excavation. OSHA requires that Type "C" material must be benched at a 1-1/2 Horizontal: 1 Vertical (1-1/2H: 1V) slope for temporary excavations. Excavations in rock may be performed with steeper slopes depending on the orientation of fractures and stability observed during excavation; a qualified person should determine proper sloping during earthwork operations at the site.

6.2 Control of Water

Groundwater was not observed during the site investigation. Groundwater seepage into open excavations is not anticipated at this time. However, the contractor should be prepared to control potential water conditions in order to maintain a stable subgrade for construction activities and the integrity of the natural bearing rock or soil.

During foundation construction and fill placement, temporary swales and ditches may be necessary to control surface water that could potentially runoff into open excavation and maintain a dry excavation for foundation construction.

Upon completion of fill placement, the final grade should be set to promote positive drainage away from the building. Topsoil with more than 20% fines will limit infiltration of surface water into the subgrade.

7.0 CLOSURE

This report and the recommendations contained herein have been prepared for the exclusive use of Higher Ground Country Club Management Company, LLC and its representatives for specific application to the design and construction of the three proposed hotel structures at the Silo Ridge Golf Resort Community in the Town of Amenia, Dutchess County, New York.

This report was prepared in accordance with generally accepted soil and foundation engineering practices. No other warranty, expressed or implied, is made. The analysis, designs and recommendations submitted in this report are based in part upon the data obtained from subsurface explorations available at the time of this report. The nature and extent of variations between these explorations may not become evident until construction. If significant variations then appear, it may be necessary to reevaluate the recommendations of this report.

Soil samples collected during the subsurface investigation are currently stored at TCC's facilities and will be retained until September 30, 2006, the discard date. If a representative does not inquire about the samples prior to the discard date, the samples shall be removed from TCC's facilities and disposed of appropriately.

We recommend that TCC be retained to:

- 1. Design site specific temporary excavation support, if necessary,
- 2. Prepare or review contract documents pertaining to site work and foundations, and
- 3. Provide construction monitoring to observe compliance with design assumptions and to facilitate design changes in the event that subsurface conditions differ from those anticipated.

The estimated fees and detailed scope of services for these additional tasks can be provided at your request.

Please feel free to contact us at (518) 273-0055 if you have any questions. TCC looks forward to working with you on this project

Sincerely,

Matthew A. Korn, EIT

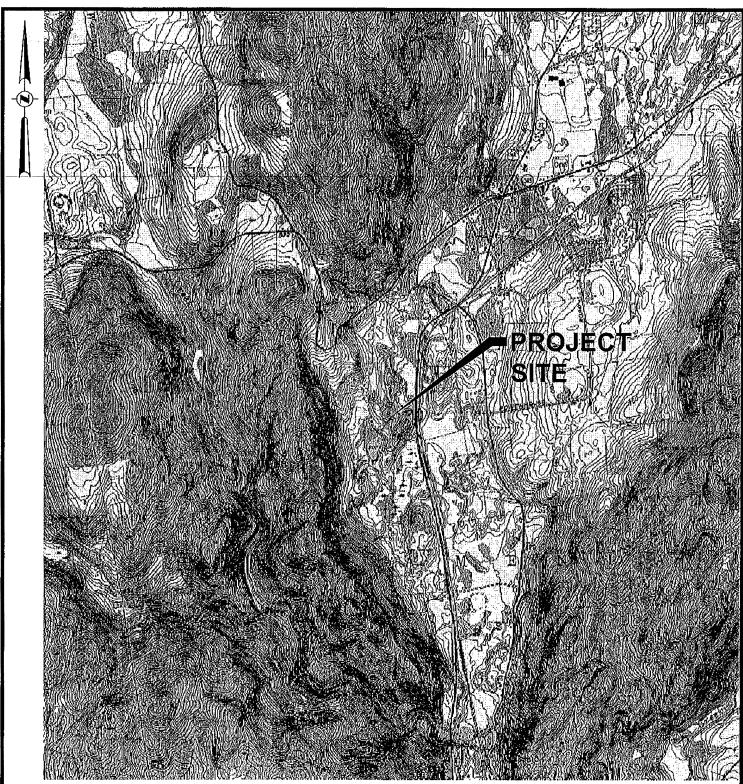
Project Geotechnical Engineer

Kevin B. O'Malley, P.E.

Director of Geotechnical

Engineering Services

Figures



ALTERATION OF THIS DRAWING, EXCEPT BY A LICENSED P.E. IS ILLEGAL. ANY ALTERATION BY A P. MUST BE INDICATED AND BEAR THE APPROPRIATE SEAL, SIGNATURE AND DATE OF ALTERATION.



Planners Environmental Scientists Dutchess County Office: 21 Fox Street Poughkeepsie, NY 12601 Phone: (845) 454-3980

Capital District Office: 547 River Street Troy, NY 12180 Phone: (518) 273-0055

Orange County Office: 356 Meadow Avenue Newburgh, NY 12550 Phone: (845) 567-1133

North Country Office: 100 Clen Street Clens Falls, NY 12801 Phone: (518) 812-0513

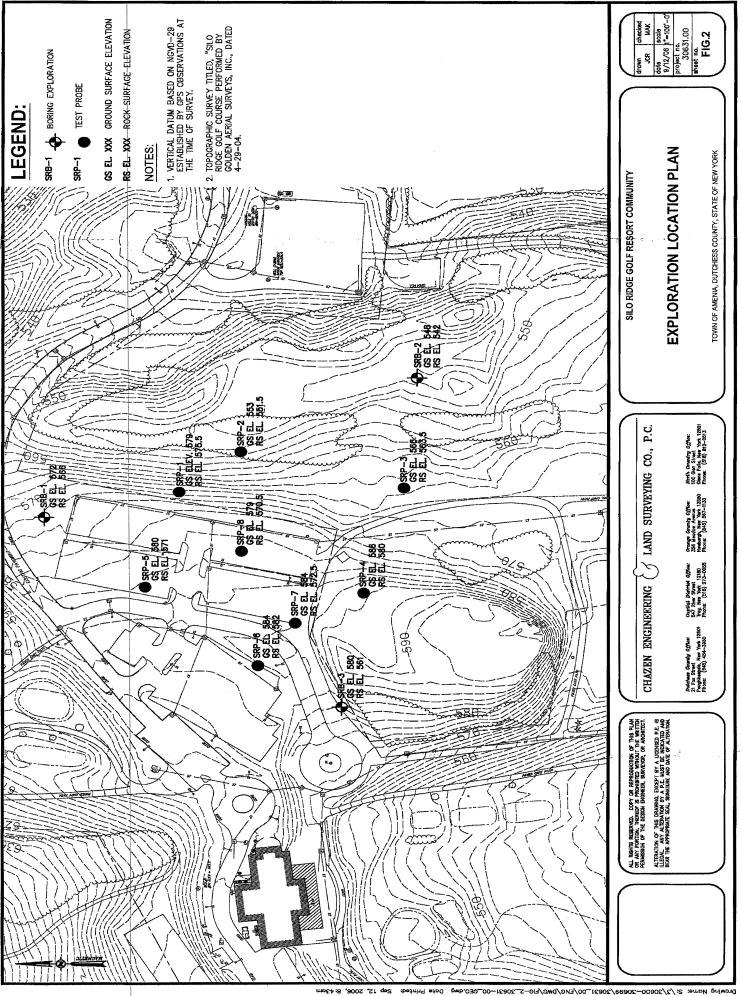
SILO RIDGE GOLF RESORT COMMUNITY

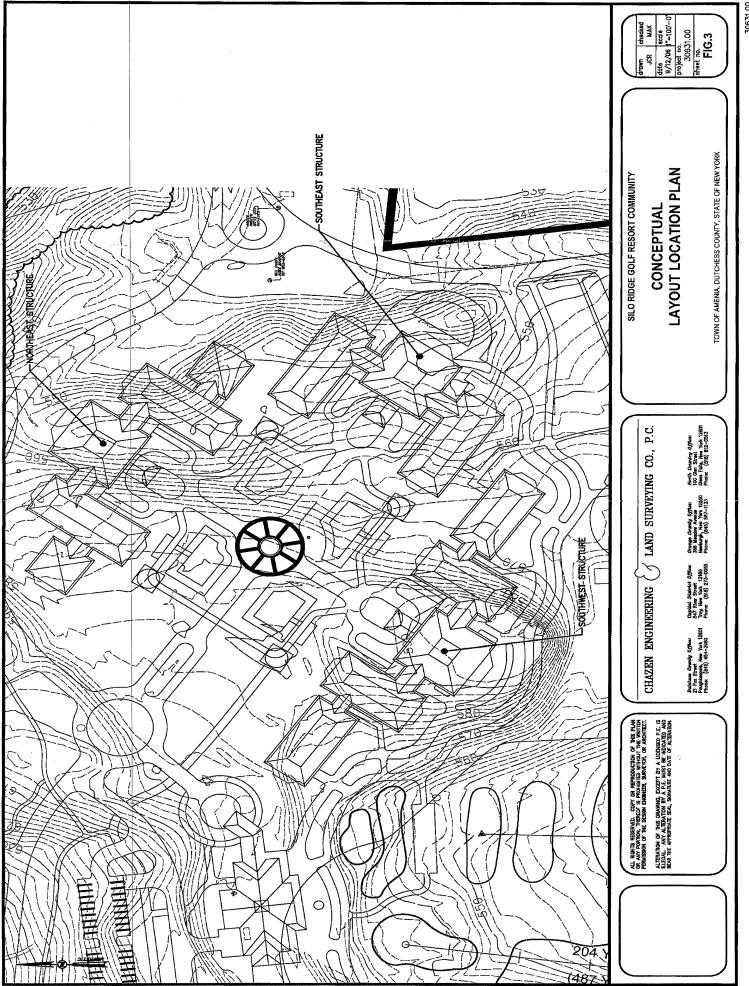
SITE LOCATION MAP

TOWN OF AMENIA, DUTCHESS COUNTY, STATE OF NEW YORK,

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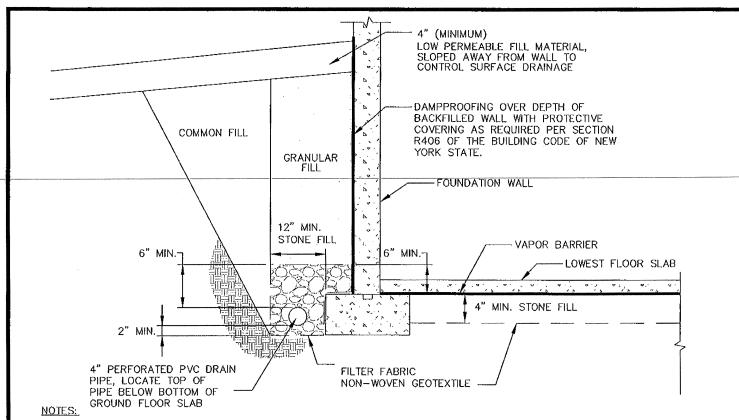
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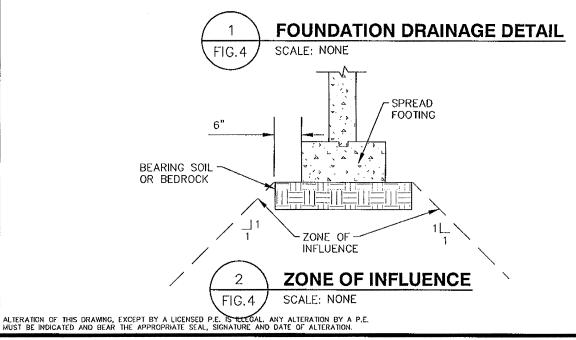


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30631.00



- 1. LOOP FOUNDATION SYSTEM DRAIN PIPE TO PROVIDE FOR ALTERNATE FLOW ROUTES IN THE EVENT OF A LOCALIZED PIPE BLOCKAGE AND PROVIDE POSITIVE DISCHARGE BY GRAVITY OR OTHER MEANS TO AN APPROVED SUBSURFACE SYSTEM.
- 2. FOUNDATION DRAIN PIPE CONSTRUCTION AS PER BUILDING CODE OF NEW YORK STATE SECTION R405.





Dutchess County Office: 21 Fox Street Poughkeepsie, NY 12601 Phone: (845) 454-3980

Capital District Office: 547 River Street Troy, NY Phone: (518) 273-0055 12180

Orange County Office: 356 Meodow Avenue Newburgh, NY 12550 Phone: (845) 567-1133

North Country Office: 100 Glen Street Glens Falls, NY 12801 Phone: (518) 812-0513

SILO RIDGE GOLF RESORT COMMUNITY

FOUNDATION DETAILS

FOWN OF AMENIA, DUTCHESS COUNTY, STATE OF NEW YORK

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JCR	MAK		
date	scale		
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Appendix A: Exploration Logs

ROCK CLASSIFICATIONS

Rock Classifications are visual descriptions on the basis of the Driller's, Technician's, Geologist's or Geotechnical Engineer's observations of the coming activity and the recovered samples applying the following classifications.

	CLASSIFICATION TERM	DESCRIPTION		
\boxtimes				
Very Hard Unable to scratch with		Unable to scratch with a knife		
Hardness	Hard	Difficulty scratching with a knife		
rdr	Medium Hard	Able to groove 1/16" with a knife		
Ha	Soft	Easily grooved with a knife		
,	Very Soft	Easily scratched with a fingernail		
\geq				
<u>8</u>	Fresh	No visible signs of rock weathering		
Weathering	Slightly Weathered	Fresh rock with staining at joints		
the	Moderately Weathered	Less than ½ of rock is discolored or weathered		
Vea	Highly Weathered	More than ½ of rock is discolored or weathered		
Completely Weathered All rock material deco		All rock material decomposed to soil, structure intact		
$\geq \leq$				
9	Amorphous	Too small to be seen with naked eye		
tal	Fine Grained	Barely seen with naked eye to 1/8"		
Texture	Coarse Grained	1/8" to 1/4"		
L	Very Coarse Grained	Greater than 1/4"		
$\geq \leq$				
ا 🔍	Horizontal	0-5°		
g	Shallow	6 – 20°		
Attitude	Moderate Dipping	21 – 45°		
Atı	Steep Dipping	46 – 85°		
	Vertical	86 – 90°		

Visual observation of the fracture joints should be described as either clean, stained or filled (clay, mineral vein or other) and noted as to whether they are rough, irregular or smooth.

Core sample RECOVERY (REC) is expressed as percent of recovered of total sampled. The ROCK QUALITY DESIGNATION (RQD) is the total length of core sample pieces exceeding 4 in. in length divided by the total interval cored for N size cored.

GENERAL

- Soil and Rock classifications are made visually on samples recovered. The presence of Gravel, Cobbles and Boulders will influence sample recovery classification density/consistency determination.
- Groundwater, if encountered, was measured and its depth recorded at the time and under the conditions as noted.
- Topsoil or pavements, if present, were measured and recorded at the time and under the conditions as noted.
- Stratifications Lines are approximate boundaries between soil types. These transitions may be gradual or distinct and are approximated.

INTERPRETATION OF SUBSURFACE LOGS

The Exploration Logs present observations and the results of tests performed in the field by the Driller, Technician, Geologists, and Geotechnical Engineers as noted. Soil/Rock classifications are made visually and modified accordingly based on laboratory results. The classification of soils or soil like material is subject to limitations imposed by the size of the sampler, the size of the sample and it's degree of disturbance and moisture.

The following defines some of the terms utilized in the preparation of the Subsurface Logs.

SOIL CLASSIFICATIONS

Soil classifications are visual descriptions on the basis of the United Soil Classification ASTM D-2488. The soil density or consistency is based on the penetration resistance determined by ASTM D 1586. Soil Moisture of the recovered materials is described as DRY, MOIST, WET or SATURATED.

SIZE DESCRIPTION		RELATIVE DENSITY/CONSISTENCY (BASIS ASTM D1586)			
Soil Type	Particle Size	Granular Soil		Cohesive Soil	
Boulder	>12"	Density	Blows/FT	Consistency	Blows/FT
Cobble	3"- 12"	Very Loose	< 4	Very Soft	< 2
Gravel-Coarse	3" – ¾"	Loose	5 - 10	Soft	2 - 5
Gravel-Fine	¾" - #4	Medium Dense	11 – 30	Medium Stiff	6 - 10
Sand-Coarse	#4 - #10	Dense	31- 50	Stiff	10 - 20
Sand-Medium	#10 - #40	Very Dense	50+	Very Stiff	20 - 30
Sand-Fine	#40 - #200			Hard	>30
Silt/NonPlastic	< #200				
Clay/Plastic	< #200				

SOIL STRUCTURE		RELATIVE PROPORTION OF SOIL TYPES		
Structure Description		Description	% of Sample by Weight	
Layer	6" Thick or Greater	Mostly	50 - 100	
Seam	6" Thick or Less	Some	30 - 45	
Parting	Less than ¼" thick	Little	15 - 25	
Varved Uniform horizontal		Few	5 - 10	
partings or seams		Trace	Less than 5	

Additional Notes:

- 1. Utilized c: coarse, m: medium, and f: fine when describing the size of sand or gravel.
- WOH weight of hammer.
- 3. WOR weight of rods.
- 4. bgs below ground surface
- 5. NA Not Available
- 6. ▼ Phreatic Surface, if observed

Refusal:

- 1. Split-spoon refusal is considered 50 blows over six inches.
- 2. Auger and Casing refusal occurs if the driller is unable to advance the boring.
- 3. Roller bit refusal occurs if the bit is worn and needs to be replaced or the bedrock is a dense very hard material.

TH	łE				547 R	liver	Street	:	PROJECT: Silo Ridge Country Club		
(a	zen		Troy,	New	York	12180	LOCATION: Town of Amenia, Dutchess County, New York	Test Boring No.: SRB-	1
C			NIES) 273-		CLIENT: Silo Ridge Country Club		
				SJB Sei) 273-	8391	PROJECT NO.: 30631.00 Start Date: August 7, 2006 Northing: See Figure 2	Total Depth: 10.5 ft Borehole Dia.: 7.25 in	n.
				CME-5				;	Finish Date: August 7, 2006 Easting: See Figure 2		ì. :
				John Le					El. Datum: NGVD29 Longitude:	Rock Depth: 10.5 ft	t
	In	spe	ctor:	Pete Ste	enland	d		:	G.S. Elevation: 572 Latitude:	Sample Hammer: Automatic	c
	<u>i</u> j		_g_			-2	-6-	<u>z</u>			
£	3	Elevation (r.)	Casing Blows	Sample No.	SPT Blows	Recovery(in)	Groundwater	Symbol			
Depth (Ft)	3	evan	ing	nple	<u> </u>	ove	JU III	Group	Stratum and		
Del	Ģ	Š	Ö		المستشارين		Ğ		Field Descriptions:	Field Notes, Comments:	
		_		SS-1	14	24		GP-GM	Poorly Graded Gravel with Silt and Sand (GP-GM): Mostly gravel, some sand, little silt, gray, dry (Highly Weathered Rock)		
,	5	71			33 91				4 inch Quartz seam		
	-	-			50				Then Quare scam		
2	5:	70									
,	- 5	69									
						ļ					•
1	5	68									
	-				 	 	 	-			
5		67		SS-2	50/4"	3		SP-SM	Poorly Graded Sand with Silt and Gravel (SP-SM): Mostly sand,	Auger Refusal at 5.5' - begin cori	ng
6		66	^	RC-1		60		1	some gravel, little silt, gray, dry (Highly Weathered Rock)		
	<u> </u>					-		N /	(5.5' to 10.5') Gneiss: very soft to hard, highly to slightly weathered, fine	REC for RC-1 = 100%	
7	5	65			-	ļ	-	$\{ \setminus I \}$	to coarse grained, horizontal bedding, gray and white, joints are iregular and smooth	RQD for RC-1 = 10 % RQD - one piece at 6"	
	-							1 V	and shooth	nego one proce at c	
8	- 5	64						1 1			
9		63						$1/\Lambda$			
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10	_ 5	62						∦ \			
							-	<u> </u>	Test Boring Terminated at 10.5 feet in Bedrock.		
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	<u> </u>						-				
19	├ ⁵	553			-	-		 -	1		
20	- -,	552									
									tary Wash, SSA- Solid Stem Auger, CPT- Cone Penetrometer	DRILLING INFORMATIO	
									Spoon, RC-Rock Core, GS-Grab, ST-Shelby Tube, PS-Piston	Method: HSA 0 to 5 Method: RC 5.5 to	
STAI		KL)							ith ASTM D-2488 unless otherwise noted. Each subsequent page: Additional 25 feet.	The second secon	Core
	*								urface Logs" for additional symbology and abbreviation definitions.		NX
ADD	ITIC	ON								Int Diam. 3.25 " 2"	2"
NOT	ES:									Weight 140 lb	
<u> </u>									·	Fall 30"	

TH CC	E Shar DMPA	<u> </u>	-	Phn:	New (518)		12180 0055	PROJECT: Silo Ridge Country Club LOCATION: Town of Amenia, Dutchess County, New York CLIENT: Silo Ridge Country Club PROJECT NO.: 30631.00	Test Boring No.: SRB-2 Total Depth: 15.8 ft.
	Dril Di	l Rig: iller:	SJB Ser CME-5 John Le Pete Ste	rvices I 50X A conharc	nc. TV it) 413-	:	Start Date: August 8, 2006 Northing: See Figure 2 Finish Date: August 8, 2006 Easting: See Figure 2 El. Datum: NGVD29 Longitude: G.S. Elevation: 548 Latitude:	Borchole Dia.: 7.25 in. Water Depth: NA ft. Rock Depth: 6 ft. Sample Hammer: Automatic
Depth (Ft)	Elevation (Ft)	Casing Blows	Sample No.	SPT Blows	Recovery(in)	Groundwater	Group Symbol	Stratum and Field Descriptions:	Field Notes, Comments:
2	— 547 — 546		SS-1	8 18 43 50/3"	17	4* with Talantina states ou	SP-SM	Poorly Graded Sand with Silt and Gravel (SP-SM): Mostly sand, some gravel, little silt, gray, dry (Highly Weathered Rock)	Moisture Content - 1.2%
3	— 545 — 544								
5 - 6 - 7 -	- 543 - 542 - 541		SS-2	16 50/3"	49		SP-SM	Poorly Graded Sand with Silt and Gravel (SP-SM): Mostly sand, some gravel, little silt, gray, dry (Highly Weathered Rock) (5.8'-10.8') Gneiss: medium hard to hard, moderately to slightly weathered, coarse to fine grained, horizontal bedding, gray and white, joints have very little staining and are irregular and smooth	Auger Refusal at 5.8' - begin coring REC for RC-1 = 81.7% RQD for RC-1 = 0%
9	540 539 538						$\left \right\rangle$		
11	537		RC-2		57		/ \	(10.8'-15.8') Gneiss: hard, slightly weathered, coarse to fine grained, horizontal bedding, gray and white, joints have very little staining and are irregular and smooth	REC for RC-2 = 95% RQD for RC-2 = 26.7%
13 - 14 -	- 535 - 534 - 533						$\left \right\rangle$		RQD - 3 pieces over 4" totaling 16"
. 16	- 532 - 531							Test Boring Terminated at 15.8 feet in Bedrock.	
18 19	- 530 - 529 - 528								
MET SAM STAN NOT	HODS PLE T NDARI ES:	YPES: 2. To 3. Ro	AS-Au imples o est Borii	uger, W classific ng Log	VS-W ed in Page	ash, S accord	S-Split lance wi 20 feet.	lary Wash, SSA- Solid Stem Auger, CPT- Cone Penetrometer Spoon, RC-Rock Core, GS-Grab, ST-Shelby Tube, PS-Piston ith ASTM D-2488 unless otherwise noted. Each subsequent page: Additional 25 feet. arface Logs" for additional symbology and abbreviation definitions.	DRILLING INFORMATION Method: HSA 0 to 5.8 Method: RC 5.8 to 15.8 Casing Sample Core Type HSA SS NX Int Diam. 3.25 " 2" 2" Weight 140 lb 140 lb Fall 30"

								1EST DUKING LUG	1 ago 1 of 2
Th	~~~			547 R				PROJECT: Silo Ridge Country Club	
(sha	zen	<u>.</u>				12180	LOCATION: Town of Amenia, Dutchess County, New York	Test Boring No.: SRB-3
C	OMPA	MIES	5		•	273		CLIENT: Silo Ridge Country Club	Tráil Donatha
	Cont	actor.	SJB Se) 273-	0271	PROJECT NO.: 30631.00 Start Date: August 8, 2006 Northing: See Figure 2	Total Depth: 29 ft. Borehole Dia.: 7.25 in.
			CME-5					Start Date: August 8, 2006 Rortning: See Figure 2 Finish Date: August 8, 2006 Easting: See Figure 2	Water Depth: NA ft.
i		-	John La					El. Datum: NGVD29 Longitude:	Rock Depth: 19 ft.
			Pete Ste				:	G.S. Elevation: 580 Latitude:	Sample Hammer: Automatic
							-5		
9	Elevation (Ft)	Casing Blows	.0	S	(in)	Groundwater	Symbol		
Depth (Ft)	atio	g B	Sample No.	SPT Blows	Recovery(in)	ng w	b S		
ept	lev	asin	amp	E	9	io.	Group	Stratum and Field Descriptions:	Field Notes, Comments:
		0 '	SS-1	3	15	G	Silty Sand (SM): Mostly sand, some silt, few gravel, trace clay, brown,	Moisture Content - 9.9%	
			- 55 1	3	"		SM	dry	
1	579			4					
2	- C2P			7					
	578								
3	577			ļ					
	-	ļ							
4	576	ļ	00.0	3	1		CNA	Other Count (OM). Months and a sure 19 C	
	-	-	SS-2	4	1		SM	Silty Sand (SM): Mostly sand, some silt, few gravel, trace clay, brown, dry	
5	575			5	 	-		J*** 7	
		ļ 		6					Cobble encountered at 6 feet
δ	574								
,	573		What rums						
8	572								
	-			ļ					
ا و	- 571	ļ	60.2		00		OD OM	Poorly Graded Sand with Silt and Gravel (SP-SM): Mostly sand, some	Approximate Strata change
			SS-3	7 8	20		SP-SIM	gravel, little silt, gray, dry (Completly Weathered Rock)	
10	570	ļ		14				<i>g </i>	
				14					
11	569								
12	568								
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13	567				ļ				
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14	- 566	ļ	SS-4	14	18		QD,QM	Poorly Graded Sand with Silt and Gravel (SP-SM): Mostly sand, some	
	-		±3°4	16	10		21 -0141	gravel, little silt, gray, dry (Highly Weathered Rock)	
15	565			50/5"				,	
,,	_ ~~								
16	564								
17	 563								1
				ļ	-	<u></u>			ļ
18	562	 							
	-				-	ļ			Auger Refusal at 19.0' - begin coring
19	561	 -	RC-1	-	31	-	\		
20	560				<u></u>		X		
MET	HODS	HSA	- Hollov	v Stem	Aug	er, RV	VH- Rot	ary Wash, SSA- Solid Stem Auger, CPT- Cone Penetrometer	DRILLING INFORMATION
SAM	PLE T	YPES:	AS-A	iger, V	vs-W	ash, S	S-Split S	Spoon, RC-Rock Core, GS-Grab, ST-Shelby Tube, PS-Piston	Method: HSA 0 to 19
			•					th ASTM D-2488 unless otherwise noted.	Method: RC 19 to 29
NOT	ES:			-	_			Each subsequent page: Additional 25 feet.	Casing Sample Core
700	YOU'S		efer to th	ne "Into	erpret	ation	of Subsu	rface Logs" for additional symbology and abbreviation definitions.	Type HSA SS NX
	ITION.	AL							Int Diam. 3.25 " 2" 2"
NOT	E-D:								Weight 140 lb
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									TEST BORING LOG	Page 2 of 2
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			ızer	2				12180		Test Boring No.: SRB-3
$\frac{1}{c}$	<u>~</u>	MAC	ANIE	<u> </u>			3) 273-		CLIENT: Silo Ridge Country Club	
7		//Y\L	VIVIC	<u>. </u>	Fax:	(518) 273-	8391	PROJECT NO.: 30631.00	Total Depth: 29 ft.
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(1.1) mdad		žť.	1 8] ej	Blo	Ver	þi.	Set	Stuatum and	
3		Elevation (Ft)	Casing Blows	Sample No.	SPT Blows	Recovery(in)	Groundwater		Stratum and Field Descriptions:	Field Notes, Comments:
_	-		10	S	S	18	10			REC for RC-1 = 51.7%
	┝╶			<u> </u>	 	-	 	1\ /	coarse to fine grained, horizontal bedding, gray and white, joints are	RQD for RC-1 = 0%
'	┝	559		-		-	 	$ \setminus $	irregular and smooth with a slight silt coating	I STORIES TO STORIES
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	Γ	557					1	/ \		
		556						V\		
		 	[RC-2	[28		\ /	(24'-29') Gneiss: medium hard to hard, highly to moderatley weathered,	
	Ĺ	555						1\ /	coarse to fine grained, horizontal bedding, gray and white, joints are	REC for RC-2 = 46.7%
	ļ.					_	ļ	$1 \setminus I$	irregular and smooth	RQD for RC-2 = 0%
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	-	551		<u> </u>		<u> </u>	t		Test Boring Terminated at 29 feet in Bedrock.	
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TH				547 R				PROJECT: Silo Ridge Country Club	Drobo No :	CDD	1
7		zen				7 ¥o rk 3) 273-	0055	LOCATION: Town of Amenia, Dutchess County, New York CLIENT: Silo Ridge Country Club	Probe No.:	SRP	-1
<u>C</u> (OMPA	MIES) 273-		PROJECT NO.: 30631.00	Total Depth:	3.5	ft.
	Contra	actor:	SJB Se				· · · · · · · · · · · · · · · · · · ·	Start Date: August 7, 2006 Northing: See Figure 2	Borehole Dia.:	7.25	in.
			CME-5					Finish Date: August 7, 2006 Easting: See Figure 2	Water Depth:	NA	ſt.
	D	riller:	John Le	eonhar	dt			El. Datum: NGVD29 Longitude:	Rock Depth:	3.5	ſt.
	Insp	ector:	Pete Ste	eenland	jt			G.S. Elevation: 579 Latitude:			
-	E	\$ <u>-</u>		ļ	-	a	<u> </u>				
Ft)	Elevation (F_ℓ)	Casing Blows	Sample No.	DWS	Recovery(in)	Groundwater	Symbol				
Depth (Ft)	vati	ing	ıple	SPT Blows	ove	und	Group	Stratum and			
Dep	Ele	Cas	San	SFI	Rec	Ę,	S.	Field Descriptions:	Field Notes, Comm	ents:	
							SM	Silty Sand (SM): Mostly sand, some silt, few gravel, trace clay, brown,			
,	- 578				ļ	<u> </u>		dry			
ŀ										.	
2	- 577				-	<u> </u>	SD.SM	Poorly Graded Sand with Silt and Gravel (SP-SM): Mostly sand, some	Approximate strata o	nange	
ŀ	•				 	 	21 -0141	gravel, little silt, gray, dry (Highly Weathered Rock)			
3	- 576				 		 	,			
, [- 575							Auger Refusal at 3.5 feet on Assumed Bedrock.	1		
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6	- 573										
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19	560										
20	559										
								tary Wash, SSA- Solid Stem Auger, CPT- Cone Penetrometer	DRILLING INF		
								Spoon, RC-Rock Core, GS-Grab, ST-Shelby Tube, PS-Piston	Method: HSA Method:	0 to	3.5
STAP TOP			-					ith ASTM D-2488 unless otherwise noted. b. Each subsequent page: Additional 25 feet.	Method: Casing	Sample	Cor
	121.7+							rface Logs" for additional symbology and abbreviation definitions.	Type HSA		
DD	TION.								Int Diam. 3.25 "	*n	
TO									Weight		
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TH		,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,		547 R	iver (Street		Į.	Silo Ridge Country					CDI	
(Bas	zen					12180		Town of Amenia, I		New York	Probe No.:		SRI	′-Z
C	OMPA	NIES) 273-) 273-		PROJECT NO.:	Silo Ridge Country	Club		Total Dep	oth:	1.5	ft.
	Contro	ctor	SJB Sei		_) 213-	0371	Start Date:	August 7, 2006	Northing:	See Figure 2	Borehole D		7.25	in.
			CME-5					Finish Date:	August 7, 2006	Easting:	See Figure 2	Water De		NA	ft.
		-	John Le					El. Datum:	NGVD29	Longitude:		Rock Der		1.5	ft.
	Insp	ector:	Pete Ste	eenlanc	l			G.S. Elevation:	553	Latitude:					
	a.	_v_			_	-1:	[8								
Depth (Ft)	Elevation (Ft)	Casing Blows	Sample No.	SPT Blows	Recovery(in)	Groundwater	Group Symbol	Stratum and Field Descriptions	:			Field Notes, C	omme	nts:	,
-		۷.	<u> </u>	8	<u> </u>			Poorly Graded Sand		rel (SP-SM): Mo	stly sand, some				
,	552							gravel, little silt, gra	ay, dry (Highly We	athered Rock)					
, [4			
2	- 551			ļ				Auger Refusal at 1.	.5 feet on Assumed	Bedrock.					
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18	535														
19	534					<u> </u>	-	4							
	533			-	-			4							
20 MIET	ł	: HSA	- Hollo	w Sten	1 Ans	er, RV	WH- Ro	l otary Wash, SSA- So	lid Stem Auger, CI	T- Cone Penetro	ometer	DRILLING	G INF	ORMAT	TION
SAM	PLE T	YPES	: AS-A	uger, V	VS-W	ash, S	S-Split	Spoon, RC-Rock C	ore, GS-Grab, ST-S	Shelby Tube, PS-	Piston	Method: HS			to 1.5
) 1. S	amples	classifi	ed in	accor	dance w	rith ASTM D-2488 u	mless otherwise no	ed.		Method:			
ro <i>r</i>	ES:	2. A	uger Pr	obe Lo	g Pag	e 1:0	- 20 fee	t. Each subsequent p	page: Additional 25	feet.	daffinist	Tyme US		Sample	
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			: CME-: : John L					Finish Date: August 7, 2006 Easting: See Figure El. Datum: NGVD29 Longitude:	2 Water Dept Rock Dept	
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Depth (Ft)	Elevation (Ft)	Casing Blows	Sample No.	SPT Blows	Recovery(in)	Groundwater	Group Symbol	Stratum and		
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	Chi OMI		en Vies	***	Phn:	New (518)	York) 273-	12180 0055	PROJECT: Silo Ridge Country Club LOCATION: Town of Amenia, Dutchess County, New York CLIENT: Silo Ridge Country Club	Probe No.:	SRI	
	Con D	trac rill Dri	ctor: Rig: iller:	SJB Se CME-5 John L Pete St	rvices l 50X A conharc	inc. TV it) 273-		PROJECT NO.: 30631.00 Start Date: August 7, 2006 Northing: See Figure 2 Finish Date: August 7, 2006 Easting: See Figure 2 El. Datum: NGVD29 Longitude: G.S. Elevation: 586 Latitude:	Total Depth: Borehole Dia.: Water Depth: Rock Depth:	6 7.25 NA 6	in. ft. ft.
Depth (Ft)	Elevation (Ft)	G r) warman	Casing Blows	Sample No.	SPT Blows	Recovery(in)	Groundwater	Group Symbol	Stratum and Field Descriptions:	Field Notes, Comn	nents:	
3	58.	13							Silty Sand (SM): Mostly sand, some silt, few gravel, trace clay, brown, dry Poorly Graded Sand with Silt and Gravel (SP-SM): Mostly sand, some gravel, little silt, gray, dry (Highly Weathered Rock)	Approximate strata	change	
5 6 7	- 58 - 58 - 57 - 57	79							Auger Refusal at 6 feet on Assumed Bedrock.			
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14 15 16	- 57 - 57 - 57 - 57 - 56	71										
-		57 56 DS:							tary Wash, SSA- Solid Stem Auger, CPT- Cone Penetrometer	DRILLING IN		
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ŀ		Dril	ler: J	ohn Le	onhard	it			El. Datum: NGVD29 Longitude:	Rock De	pth:	9	ft.
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<u>~</u>	8	gl	Casing Blows	Sample No.	SPT Blows	Recovery(in)	Groundwater	, A					
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~				_) 273-	8391	PROJECT NO.:					Depth:	2	ft.
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	,	Inspe	ctor:	Pete Ste	eenland	d	r		G.S. Elevation:	584	Latitude:		ļ			
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£		Elevation (Ft)	Casing Blows	Sample No.	S.M.	Recovery(in)	Groundwater	Group Symbol								
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	OMILY	MAIL		Fax:	(518) 273-	8391	PROJECT NO.: 30631.00	Total D	epth:	8.5	ft.
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ADD	ITION	AL								.25 "	***	
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Appendix B: Laboratory Test Results



Albany 22 Corporate Drive Clifton Park, NY 12065 518/383-9144 (T) 518/383-9166 (F)

August 31, 2006

The Chazen Companies 547 River Street Troy, New York 12180

Attn: Mr. Kevin O'Malley

Re: Laboratory Test Results

Silo Ridge

Project # 30631.00

ATL Report Nos. AT354SL-268 & 270-08-06

Ladies/Gentlemen:

On August 28, 2006 you delivered two soil samples to our Clifton Park, New York facility for testing. A Moisture Content in accordance with ASTM D 2216 and a Particle Size Analysis in accordance with ASTM D 422, without hydrometer was performed on each sample. The results of these tests follow:

Moisture Content ASTM D 2216

ATL Sample Number	Client ID#	Moisture Content (%)
AT354S268	SRB-3, SS-1, 0-2 ft	9.9
AT354S270	SRB-2, SS-1, 0-2 ft	1.2

The Particle Size Analysis are enclosed.

Please contact our office should you have any questions or if we may be of further service.

Sincerely,

Atlantic Testing Laboratories, Limited

Robert E. Field Laboratory Manager

Laudiatory Wallage

RF/nd

Particle Size Distribution Report

Project: Laboratory Analysis

Report No.: AT354SL268-08-06

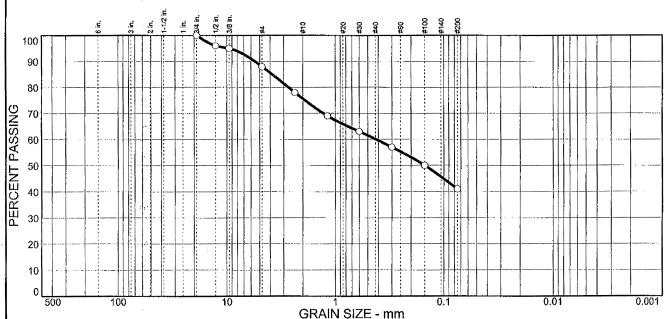
Client: The Chazen Companies

Date: 8/31/06_

Source of Sample: Silo Ridge 30631.00

Sample No: AT354\$268 Location: SRB-3, SS-1, 0-2 ft

Elev./Depth: 0-2 ft



		0/0410			O/ FINITO		
% COBBLES	% GRAVEL		% SAND		% FINES		
% COBBLES	CRS.	FINE	CRS.	MEDIUM	FINE	SILT	CLAY
0	0	12	12	16	19	41	

SIEVE	PERCENT	SPEC.*	OUT OF
SIZE	FINER	PERCENT	SPEC. (X)
0.75 in. 0.5 in. 0.375 in. #4 #8 #16 #30 #50 #100 #200	100 96 95 88 78 69 63 57 50 41		

Soil Description Brown cmf SAND, little f GRAVEL, and SILT/CLAY					
	Attaula aun Lingita				
PL=	Atterberg Limits	PI=			
D ₈₅ = 3.83 D ₃₀ = C _u =	Coefficients D60= 0.420 D15= Cc=	D ₅₀ = 0.150 D ₁₀ =			
USCS= SM	Classification AASHTC)= A-4(0)			
Remarks Sample delivered by the client on 8/28/06. ASTM D 422 without hydrometer.					

Moisture Content = 9.9%

(no specification provided)

-ATLANTIC TESTING LABORATORIES, LIMITED-

Reviewed by: .

Date: 8/3/06

Particle Size Distribution Report

Project: Laboratory Analysis

Report No.: AT354SL270-08-06

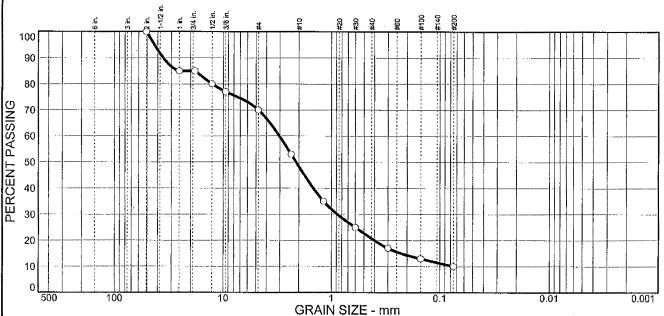
Client: The Chazen Companies

Date: 8/31/06

Source of Sample: Silo Ridge 30631.00

Sample No: AT354S270 **Location:** SRB-2, SS-1, 0-2 ft

Elev./Depth: 0-2 ft



% COBBLES	% GRAVEL		% SAND			% FINES	
70 COBBLES	CRS.	FINE	CRS.	MEDIUM	FINE	SILT	CLAY
0	15	15	22	28	10	10	

SIEVE	PERCENT	SPEC.*	OUT OF
SIZE	FINER	PERCENT	SPEC. (X)
2 in. 1 in. 0.72 in. 0.5 in. 0.375 in. #4 #8 #16 #30 #50 #100 #200	100 85 85 80 77 70 53 35 25 17 13		

	Attorbora Limita	
PL=	Atterberg Limits	PI=
D ₈₅ = 18.3 D ₃₀ = 0.881 C _u = 40.46	Coefficients D ₆₀ = 3.03 D ₁₅ = 0.227 C _c = 3.41	D ₅₀ = 2.12 D ₁₀ = 0.0750
USCS= SP-SM	Classification AASHT	O= A-1-a

Soil Description

(no specification provided)

ATLANTIC TESTING LABORATORIES, LIMITED-

Moisture Content = 1.2 %

8/31/06 Reviewed by: _ Date: __



ATLANTIC TESTING LABORATORIES

22 Corporate Drive Clifton Park, NY 12065 518/383-9144 (T) 518/383-9166 (F)

September 08, 2006

-The Chazen-Companies-547 River Street Troy, New York 12180

Attn.: Mr. Kevin O'Malley

Re:

Rock Core Compression Test

Silo Ridge

Chazen Project No. 30631-00 ATL Report No. AT354N-02-08-06

Ladies/Gentlemen:

On August 28, 2006, a representative of the Chazen Companies delivered one 2-inch rock core sample to our Clifton Park, New York facility for testing. The samples were tested for compressive strength in general accordance with ASTM D 2938. The results are as follows:

Compression Results ASTM D 2938

Core Identification	Core Length	Core Diameter (in.)	Core Area (in.²)	Total Load (lbs.)	Compressive Strength (psi)	L/D Capped (inches)	L/D Correction Factor	Corrected Unit Load (psi)
SRB-2, RS-1	3.877	1.938	2.95	13,980	4739	2.00	1.00	4740

Break Descriptions

Core Identification	Description
SRB-2, RS-1	Sheared on bedding plane

Please contact our office should you have any questions on this report, or if we may be of further service.

Respectfully,

ATLANTIC TESTING LABORATORIES, Limited

Robert E, Field Laboratory Manager bfield@atlantictesting.com

REF/nd